

**UNIVERSITY COLLEGE TATI (UC TATI)****FINAL EXAMINATION QUESTION BOOKLET**

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| COURSE CODE | : BCE 2214 |
| COURSE | : UNIT OPERATION 1 |
| SEMESTER/SESSION | : 2-2023/2024 |
| DURATION | : 3 HOURS |

Instructions:

1. This booklet contains 5 questions. Answer **ALL** questions.
2. All answers should be written in answer booklet.
3. Write legibly and draw sketches wherever required.
4. If in doubt, raise your hands and ask the invigilator.

**DO NOT OPEN THIS BOOKLET UNTIL YOU ARE TOLD TO DO SO
YOU ARE PERMITTED TO BRING ONE SHEET, EQUIVALENT TO TWO
PAGES ON AN A4-SIZED PAPER**

THIS BOOKLET CONTAINS 11 PRINTED PAGES INCLUDING COVER PAGE

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QUESTION 1

A gas mixture with a total pressure of 2.026×10^5 Pa, consisting of air and SO_2 , is brought into contact with pure water in a single-stage equilibrium mixer at a temperature of 293 K. The partial pressure of SO_2 in the original gas is 1.52×10^4 Pa. The inlet gas contains a total of 5.70 kg mol, while the inlet water contains a total of 2.20 kg mol. The exit gas and liquid leaving the mixer are in equilibrium. Figure 1 provides the equilibrium data required to answer the following questions:

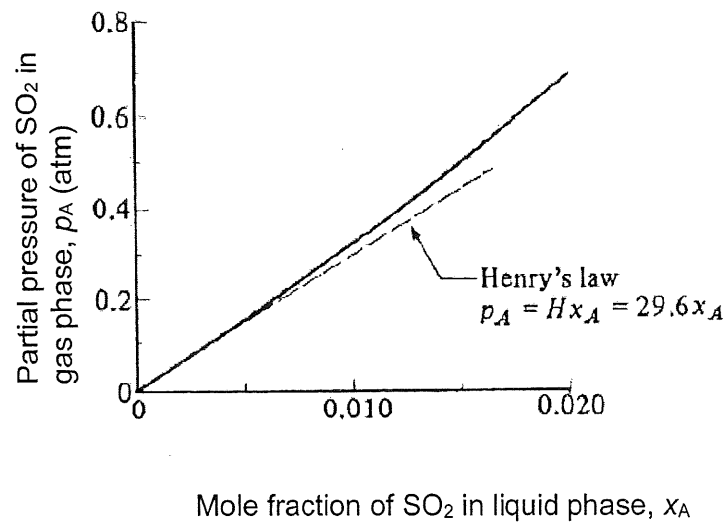


Figure 1: Equilibrium plot for SO_2 -water system at 293 K (20°C).

- Illustrate the diagram for this process (3 marks)
- Convert total pressure to atm unit (2 marks)
- Find the value of y_{A2} (2 marks)
- From Henry's Law equation in Figure 1, employ the equation of y_{A1} in terms of x_{A1} (3 marks)
- Compute x_{A1} , y_{A1} , $L1$ and $V1$ (10 marks)

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QUESTION 2

An evaporator with an area of 83.6 m^2 and a heat transfer coefficient (U) of $2270 \text{ W/m}^2\cdot\text{K}$ is employed to generate distilled water for a boiler feed. The feed to the evaporator is tap water, which contains 400 ppm dissolved solids and is at a temperature of 15.6°C . The evaporator operates at an absolute pressure of 1 atm. Saturated steam at a temperature of 115.6°C is accessible for heating. The outlet liquid contains 800 ppm solids. Assume: Datum temperature is 100°C and the heat capacity of feed is $4.188 \text{ kJ/kg}\cdot\text{K}$.

- a) Describe the process with suitable diagram (5 marks)
- b) Interpret the mass balance and find V in terms of F (3 marks)
- c) Discover the latent heat of water and steam from the steam table (4 marks)
- d) Compute the value of F (kg/h) and V (kg/h distilled H_2O) (8 marks)

QUESTION 3

- a) The air entering a dryer has a temperature of 65.6°C (150°F) and a dew point of 15.6°C (60°F).
 - i) Use humidity chart to solve the actual humidity in SI unit. (2 marks)
 - ii) Use humidity chart to compute percentage humidity. (2 marks)
 - iii) Solve the humid volume of this mixture in SI unit (4 marks)
 - iv) Solve humid heat in SI unit (4 marks)

- b) The air in a room has a humidity H of $0.021 \text{ kg H}_2\text{O/kg dry air}$ at 32.2°C and 101.3 kPa with a partial pressure, $p_A = 3.309 \text{ kPa}$. Compute the following:
 - i) Percentage humidity H_P (6 marks)
 - ii) Percentage relative humidity H_R (2 marks)

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QUESTION 4

An enriching tower is fed 100 kg mol/h of a saturated vapor feed containing 40 mol % benzene (A) and 60 mol % toluene (B) at 101.32 kPa abs. The distillate is to contain 90 mol % benzene, while the bottom contain 27.5 mol % benzene. The reflux ratio is set at 4.0:1.

- a) Compute the kg mol/h distillate, D. (3 marks)
- b) Compute the kg mol/h bottoms, W. (2 marks)
- c) Solve q and slope. Justify your answer. (3 marks)
- d) Sketch q line and enriching operating line in equilibrium diagram for benzene-toluene at 101.32 kPa (1 atm) in page 11 (6 marks)
- e) Compute the number of theoretical trays needed. (6 marks)

QUESTION 5

- a) Describe three (3) applications of each, leaching and liquid-liquid extraction in chemical process industries (6 marks)
- b) A slurry of flaked soybeans weighing a total of 100 kg contains 75 kg of inert solids and 25 kg of solution with 10 wt % oil and 90 wt % solvent hexane. This slurry is contacted with 100 kg of pure hexane in a single stage so that the value of N for the outlet underflow is 1.5 kg insoluble solid/kg solution retained. The process flow is shown in Figure 2.

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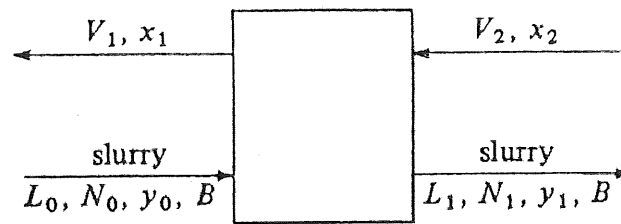


Figure 2: Process Flow

- i) Show the amount of V_2 , x_{A2} , x_{c0} , x_{c2} , L_0 , y_{A0} in Figure 2 (6 marks)
- ii) Compute total flow rate (M), ratio of solid to solution (N_0), x_{AM} and N_M (8 marks)

-----End of question-----

ATTACHMENTS

$$p_A = Hx_A$$

$$y_A = H'x_A$$

$$H' = H/P$$

$$L' \left(\frac{x_{A0}}{1 - x_{A0}} \right) + V' \left(\frac{y_{A2}}{1 - y_{A2}} \right) = L' \left(\frac{x_{A1}}{1 - x_{A1}} \right) + V' \left(\frac{y_{A1}}{1 - y_{A1}} \right)$$

$$V' = V(1 - y_A)$$

$$L_1 = \frac{L'}{1 - x_{A1}}$$

$$V_1 = \frac{V'}{1 - y_{A1}}$$

$$F = L + V$$

$$h_F = c_{pF}(T_F - T_1)$$

$$q = S(H_s - h_s) = S\lambda$$

$$Fh_F + S\lambda = Lh_L + VH_V$$

$$q = S(\lambda) = UA \Delta T$$

$$H_s = \frac{18.02}{28.97} \frac{p_{AS}}{P - p_{AS}}$$

$$H_p = 100 \frac{H}{H_s}$$

$$H_R = 100 \frac{p_A}{p_{AS}}$$

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$$c_s \text{ kJ/kg dry air} \cdot \text{K} = 1.005 + 1.88H \quad (\text{SI})$$

$$c_s \text{ btu/lb}_m \text{ dry air} \cdot ^\circ\text{F} = 0.24 + 0.45H \quad (\text{English})$$

$$\begin{aligned} v_H \text{ m}^3/\text{kg dry air} &= \frac{22.41}{273} T \text{ K} \left(\frac{1}{28.97} + \frac{1}{18.02} H \right) \\ &= (2.83 \times 10^{-3} + 4.56 \times 10^{-3} H) T \text{ K} \end{aligned}$$

$$\begin{aligned} v_H \text{ ft}^3/\text{lb}_m \text{ dry} &= \frac{359}{492} T ^\circ\text{R} \left(\frac{1}{28.97} + \frac{1}{18.02} H \right) \\ &= (0.0252 + 0.0405H) T ^\circ\text{R} \end{aligned}$$

$$L_0 + V_2 = L_1 + V_1 = M$$

$$L_0 y_{A0} + V_2 x_{A2} = L_1 y_{A1} + V_1 x_{A1} = M x_{AM}$$

$$B = N_0 L_0 + 0 = N_1 L_1 + 0 = N_M M$$

UNIT OPERATION 1 (BCE 2214)

Table A.2-9a. *Properties of Saturated Steam and Water (Steam Table), SI Units*

| Temperature (°C) | Vapor Pressure (kPa) | Specific Volume (m ³ /kg) | | Enthalpy (kJ/kg) | | Entropy (kJ/kg · K) | |
|---------------------|----------------------------|---|----------------|---------------------|----------------|------------------------|----------------|
| | | Liquid | Sat'd Vapor | Liquid | Sat'd Vapor | Liquid | Sat'd Vapor |
| 0.01 | 0.6110 | 0.0010002 | 206.14 | 0.00 | 2501.4 | 0.00 | 9.1555 |
| 10 | 1.2260 | 0.0010003 | 106.31 | 42.02 | 2519.2 | 0.1511 | 8.8998 |
| 15 | 1.7051 | 0.0010009 | 77.881 | 62.98 | 2528.4 | 0.2245 | 8.7804 |
| 20 | 2.3371 | 0.0010018 | 57.761 | 83.92 | 2537.5 | 0.2965 | 8.6661 |
| 25 | 3.169 | 0.0010030 | 43.341 | 104.84 | 2546.5 | 0.3673 | 8.5568 |
| 30 | 4.246 | 0.0010044 | 32.882 | 125.75 | 2555.6 | 0.4368 | 8.4521 |
| 35 | 5.6236 | 0.0010060 | 25.208 | 146.64 | 2564.6 | 0.5052 | 8.3518 |
| 40 | 7.384 | 0.0010079 | 19.517 | 167.54 | 2573.5 | 0.5724 | 8.2557 |
| 45 | 9.593 | 0.0010099 | 15.253 | 188.44 | 2582.5 | 0.6386 | 8.1634 |
| 50 | 12.349 | 0.0010121 | 12.028 | 209.34 | 2591.3 | 0.7038 | 8.0749 |
| 55 | 15.759 | 0.0010145 | 9.5649 | 230.24 | 2600.1 | 0.7680 | 7.9899 |
| 60 | 19.940 | 0.0010171 | 7.6677 | 251.15 | 2608.8 | 0.8312 | 7.9082 |
| 65 | 25.03 | 0.0010199 | 6.1938 | 272.08 | 2617.5 | 0.8935 | 7.8296 |
| 70 | 31.19 | 0.0010228 | 5.0397 | 293.02 | 2626.1 | 0.9550 | 7.7540 |
| 75 | 38.58 | 0.0010258 | 4.1291 | 313.97 | 2634.6 | 1.0156 | 7.6812 |
| 80 | 47.39 | 0.0010290 | 3.4053 | 334.95 | 2643.0 | 1.0754 | 7.6110 |
| 85 | 57.83 | 0.0010324 | 2.8259 | 355.95 | 2651.3 | 1.1344 | 7.5434 |
| 90 | 70.14 | 0.0010359 | 2.3591 | 376.97 | 2659.5 | 1.1927 | 7.4781 |
| 95 | 85.03 | 0.0010396 | 1.9806 | 398.02 | 2667.6 | 1.2502 | 7.4150 |
| 100 | 101.32 | 0.0010435 | 1.6719 | 419.10 | 2675.6 | 1.3070 | 7.3541 |

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|-----|--------|-----------|---------|---------|---------|---------|--------|
| 105 | 38.58 | 0.0010474 | 1.4185 | 440.21 | 2683.41 | 1.36327 | 2.2951 |
| 110 | 47.39 | 0.0010516 | 1.2094 | 461.36 | 2691.11 | 1.41877 | 2.2380 |
| 115 | 169.06 | 0.0010559 | 1.0359 | 482.55 | 2698.61 | 1.47357 | 1.827 |
| 120 | 198.53 | 0.0010603 | 0.8919 | 503.71 | 2706.31 | 1.52767 | 1.296 |
| 125 | 232.1 | 0.0010649 | 0.7706 | 524.99 | 2713.51 | 1.58137 | 0.775 |
| 130 | 270.1 | 0.0010697 | 0.6685 | 546.31 | 2720.51 | 1.63447 | 0.269 |
| 135 | 313.0 | 0.0010746 | 0.5822 | 567.69 | 2727.31 | 1.68706 | 0.9777 |
| 140 | 316.3 | 0.0010797 | 0.5089 | 589.13 | 2733.91 | 1.73916 | 0.9299 |
| 145 | 415.4 | 0.0010850 | 0.4463 | 610.63 | 2740.31 | 1.79076 | 0.8833 |
| 150 | 475.8 | 0.0010905 | 0.3928 | 632.20 | 2746.51 | 1.84186 | 0.8379 |
| 155 | 543.1 | 0.0010961 | 0.3468 | 653.84 | 2752.41 | 1.89256 | 0.7935 |
| 160 | 617.8 | 0.0011020 | 0.3071 | 675.55 | 2758.11 | 1.94276 | 0.7502 |
| 165 | 700.5 | 0.0011080 | 0.2727 | 697.34 | 2763.51 | 1.99256 | 0.7078 |
| 170 | 791.7 | 0.0011143 | 0.2428 | 719.21 | 2768.72 | 0.04196 | 0.6663 |
| 175 | 892.0 | 0.0011207 | 0.2168 | 741.17 | 2773.62 | 0.09096 | 0.6256 |
| 180 | 1002.1 | 0.0011274 | 0.19405 | 763.22 | 2778.22 | 0.13966 | 0.5857 |
| 190 | 1254.4 | 0.0011414 | 0.15654 | 807.62 | 2786.42 | 0.23596 | 0.5079 |
| 200 | 1553.8 | 0.0011565 | 0.12736 | 852.45 | 2793.22 | 0.33096 | 0.4323 |
| 225 | 2548 | 0.0011992 | 0.07849 | 966.78 | 2803.32 | 0.56396 | 0.2503 |
| 250 | 3973 | 0.0012512 | 0.05013 | 1085.36 | 2801.52 | 0.79276 | 0.0730 |
| 275 | 5942 | 0.0013168 | 0.03279 | 1210.07 | 2785.03 | 0.02085 | 0.8938 |
| 300 | 8581 | 0.0010436 | 0.02167 | 1344.0 | 2749.03 | 0.25345 | 0.7045 |
| 180 | 1002.1 | 0.0011274 | 0.19405 | 763.22 | 2778.22 | 0.13966 | 0.5857 |
| 190 | 1254.4 | 0.0011414 | 0.15654 | 807.62 | 2786.42 | 0.23596 | 0.5079 |
| 200 | 1553.8 | 0.0011565 | 0.12736 | 852.45 | 2793.22 | 0.33096 | 0.4323 |
| 225 | 2548 | 0.0011992 | 0.07849 | 966.78 | 2803.32 | 0.56396 | 0.2503 |
| 250 | 3973 | 0.0012512 | 0.05013 | 1085.36 | 2801.52 | 0.79276 | 0.0730 |
| 275 | 5942 | 0.0013168 | 0.03279 | 1210.07 | 2785.03 | 0.02085 | 0.8938 |
| 300 | 8581 | 0.0010436 | 0.02167 | 1344.0 | 2749.03 | 0.25345 | 0.7045 |

Source: Data from ASME Steam Tables, Compact Edition, © 2006 ASME.

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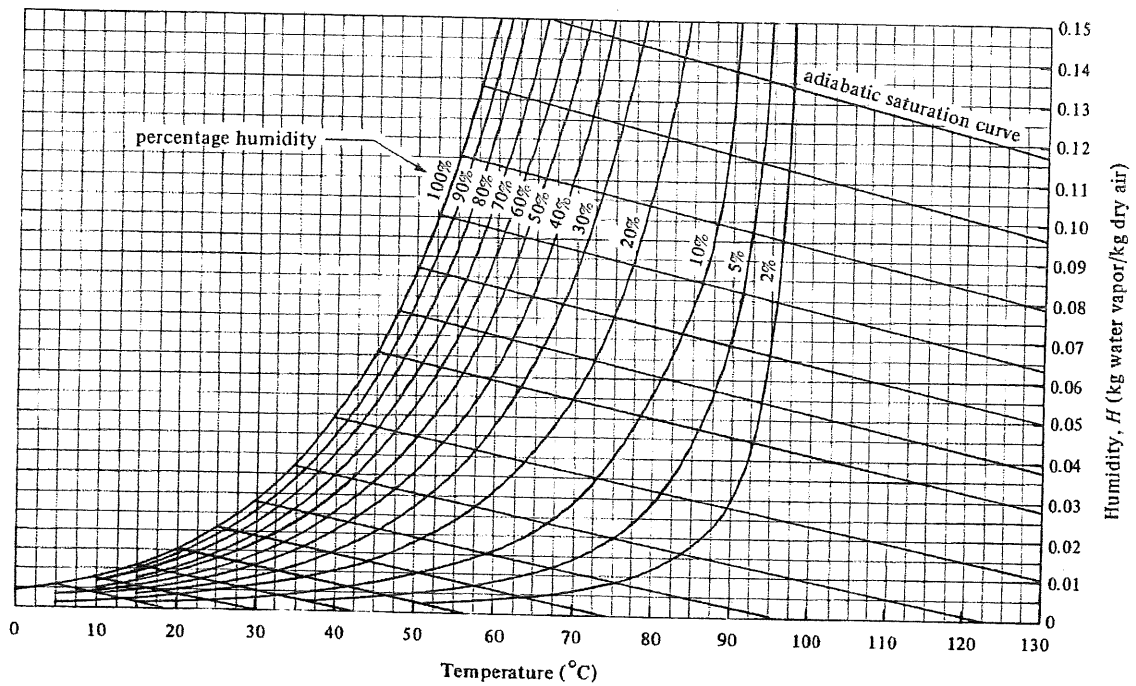


Figure 33.3-2. Humidity chart for mixtures of air and water vapor at a total pressure of 101.325 kPa (760 mmHg). From R. E. Treybal, Mass-Transfer Operations, 3rd ed. New York: McGraw-Hill Book Company, 1980. With permission.

Table A.1-19. Temperature

| |
|--|
| $0^{\circ}\text{C} = 32^{\circ}\text{F}$ (freezing point of water) |
| $1.0\text{ K} = 1.0^{\circ}\text{C} = 1.8^{\circ}\text{F} = 1.8^{\circ}\text{R}$ (Rankine) |
| $^{\circ}\text{F} = 32 + 1.8 (^{\circ}\text{C})$ |
| $^{\circ}\text{C} = (1/1.8)(^{\circ}\text{F} - 32)$ |
| $^{\circ}\text{R} = ^{\circ}\text{F} + 459.67$ |
| $\text{K} = ^{\circ}\text{C} + 273.15$ |
| $100^{\circ}\text{C} = 212^{\circ}\text{F} = 373.15\text{ K} = 671.67^{\circ}\text{R}$ |
| $0^{\circ}\text{C} = 32^{\circ}\text{F} = 273.15\text{ K} = 491.67^{\circ}\text{R}$ |
| $-273.15^{\circ}\text{C} = -459.67^{\circ}\text{F} = 0\text{ K} = 0^{\circ}\text{R}$ (absolute zero) |

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Reminder: Plot q line and enriching operating line in this diagram and submit together with your answer script.

